

NON-LINEAR CRUSTAL DEFORMATION MODELING FOR DYNAMIC REFERENCE FRAME: A CASE STUDY IN PENINSULAR MALAYSIA

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• Series of major EQ struck the Sundaland platelet since December 2004.

• The plate has been undergoing significant coseismic offset and postseismic relaxation deformation that affecting national geodetic reference frame for countries in the region such Indonesia, Malaysia, and Thailand.

Trimble







DELTA

EAST

0 -5 year 20 DELTA 15 UP 10 5 0 -5

2004 2005 2006 2007 2008 2009 2010 2011 2012 2013 2014 year

(d) Periodic signal motion (e) Random noise ward man marker w -----

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Measurement

Noise/errors

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PHASE 1: Crustal deformation trend analysis

Selection of Rigid Plate Motion of Sunda Velocity Residual 8 NNR-MORVEL56 CGPS **ITRF2008** Simon 2007 (revised) North component (mm/yr) -4 2drms: NNR-MORVEL56 = 6.4mm/yr CGPS = 5.2mm/yr ITRF2008 = 2.8mm/yr Simon 2007 = 2.3mm/yr -2 0 2 6 -8 4 East component (mm/yr)



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PHASE 2: Co- and Postseismic afterslip parameter estimation



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PHASE 2: Co- and Postseismic afterslip parameter estimation





	LOGARITHMIC (T _{north} = 148.5days)				EXPONENTIAL (T _{north} = 819.3days)			
Site	(T _{east} =204.1days)			T _{east} = 920.4days)				
	α _{north} (mm)	α _{east} (mm)	Horizontal (mm)	R ² (mm)	α _{north} (mm)	α _{east} (mm)	Horizontal (mm)	R ² (mm)
LGKW	-36.3	-116.0	121.5	0.9	-109.2	-320.0	338.1	0.9
BABH	-25.7	-87.9	91.5	1.0	-76.8	-241.1	253.0	0.9
UUMK	-26.3	-73.8	78.4	0.9	-78.6	-203.0	217.7	0.9
PUPK	-24.5	-75.4	79.3	0.9	-73.0	-206.8	219.3	0.8
SGPT	-27.7	-93.8	97.8	0.9	-83.0	-257.8	270.9	0.6
MERU	-10.1	-63.6	64.4	0.7	-30.3	-175.4	178.0	0.5
BANT	-7.8	-49.1	49.7	0.5	-23.2	-134.7	136.7	0.5
UPMS	-7.8	-49.1	49.7	0.5	-20.9	-141.2	142.8	0.5
KLAW	-6.3	-38.7	39.2	0.5	-18.7	-106.9	108.5	0.4
JUML	-4.8	-35.0	35.3	0.5	-14.3	-96.1	97.1	0.4
KUKP	-3.0	-24.2	24.4	0.4	-9.0	-66.4	67.0	0.4

Site in Peninsular Malaysia (centre line & east-coast)



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Phase 3: Resolving Dynamic Reference Frame



Phase 3: Resolving Dynamic Reference Frame



- The crustal deformation after each earthquake event is considered as the signal to be estimated.
- By adopting least square prediction technique as expressed by Moritz, (1962); and Moritz, (1980), the predicted signal S (*i.e.*, co-seismic offset, post-seismic deformation parameter and site velocity) at the nearest point.



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Phase 3: Resolving Dynamic Reference Frame

Empirical & Model Covariance Function

for each co-seismic offset, post-seismic amplitude, Sundaland's site velocity to enable for deformation signal prediction at Quasi Network Grid



Phase 3: Resolving Dynamic Reference Frame







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	Assumption	NCING THE GEOSPATIAL MATURITY OF SOCIETIES Phase 3: Resolving Dynamic Reference Frame (Assessment) Explanation	Temporal Trend of Crustal	STDM Models					
-	Assumption 1	After the occurrence of major earthquakes in Sundaland, crustal deformation in Peninsular Malaysia still induced by similar rotation of Sunda plate only.	Deformation Linear STDM and CSDM correction	Sunda plate rotation					
20	Assumption 2	After the occurrence of major earthquakes in Sundaland, crustal deformation in Peninsular Malaysia has changed and continually moving as different plate entity apart from Sunda plate rotation .	Linear STDM and CSDM correction	Fitted piece-wise linear station velocity					
	Assumption 3	After the occurrence of major earthquakes in Sundaland, crustal deformation of Peninsular Malaysia still induced by the similar rotation of Sunda plates at it was before, but undergoing significant afterslip deformation (i.e., co-seismic and post-seismic).	Non-linear STDM and CSDM correction	SuLin-STDM + PosNoLIn-STDM + CSDMs					















Phase 3: Resolving Dynamic Reference Frame (Assessment)





Concluding Remark

- The results indicate after the occurrence of major earthquakes in Sundaland, crustal deformation of Peninsular Malaysia is still induced by the similar rotation of Sunda plates as it was before, but undergoing significant afterslip deformation that depicts non-linear crustal deformation over the region.
- Therefore, the utilization of CSDM and nonlinear STDM is appropriate to cope with dynamics reference frame due to non-linear crustal deformation.

~83% of simulated CTS from Assumption 1 fall inside the 2cm limit, and ~17% fall between 2 and 4 cm. Meanwhile, 22% of simulated CTS from Assumption 2 fall within 2 cm limit, and the other 78% were distributed from 2 to 10 cm.

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